#### International Workshop "Ultrafast Beams and Applications"

## The Resonant Impedance of a Metal-Dielectric Structures in THz Region

Mikayel Ivanyan

**CANDLE SRI** 

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### Abstract

The resonant properties of the impedance of a two-layer circular metal-dielectric waveguide are investigated. Their dependence on the geometric and electromagnetic parameters of the waveguide is considered: The conditions of a single-mode nature of the radiation field of a point particle and a Gaussian bunch are established numerically.

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## Introduction

- The main source of radiation dissipation in the metal-dielectric waveguide is the finite conductivity of the metal wall and the attenuation due to the losses of dielectric (due to imaginary part of the dielectric constant of the internal dielectric coating). With an idealized consideration of the outer wall as ideally conductive and in the absence of loss in the dielectric, the movement of a particle in a waveguide will not be accompanied by a loss of energy. The impedance of the structure in this case contains only the imaginary component. The equivalent circuit of such a process corresponds to a parallel inductive-capacitive resonant oscillatory circuit without loss.
- The real model of the structure should take into account both dielectric and metal losses.

#### **2. Statement of the Problem**

A metal waveguide with an internal dielectric coating is considered.



 $\varepsilon_1, \varepsilon_2$  - relative dielectric constant of layers  $\sigma_2 = 58 \times 10^6 \ \Omega^{-1} m^{-1}$  - conductivity of copper (Cu)  $\varepsilon'_1 = 10 \ \varepsilon''_1 = 0, 0.1, 0.5 \text{ and } 3$   $a_1 = 2mm, d = a_2 - a_1, d = 200 \mu m \text{ and } d = 2 \mu m$ The cases of thick  $(\frac{d}{a_1} = 0, 1)$  and thin  $(\frac{d}{a_1} = 0, 001)$  dielectric coatings are considered.

#### Longitudinal impedance, exact formulae

$$\begin{split} \bullet \ & Z_{||} = \left\{ Z_{diel}^{-1} + Z_{rez}^{-1} \right\}^{-1} \qquad \beta_{1,2} = k\sqrt{1 - \varepsilon_{1,2}\mu_{1,2}} \\ \bullet \ & Z_{diel} = j \frac{Z_0}{\pi k a_1^2} \left[ 1 - \frac{2\varepsilon_1}{a_1\beta_1} \frac{U_3}{U_1} \right]^{-1} \qquad \varepsilon_2 = \varepsilon_0 + j \,\sigma_{1,2}/\varepsilon_0 \omega \\ \bullet \ & Z_{rez} = -j \frac{Z_0}{2\pi k \varepsilon_1} \beta_1^3 a_2 U_1 \left( U_2 + \frac{\beta_1}{\varepsilon_1} \frac{\varepsilon_2}{\beta_2} U_1 \alpha \right) \quad \varepsilon_1 = \varepsilon_1' + j \varepsilon_1'' \\ \bullet \ & U_1 = I_0(\beta_1 a_2) K_0(\beta_1 a_1) - I_0(\beta_1 a_1) K_0(\beta_1 a_2) \\ \bullet \ & U_2 = I_1(\beta_1 a_2) K_0(\beta_1 a_1) + I_0(\beta_1 a_1) K_1(\beta_1 a_2) \\ \bullet \ & U_3 = -I_0(\beta_1 a_2) K_1(\beta_1 a_1) - I_1(\beta_1 a_1) K_0(\beta_1 a_2) \\ \bullet \ & U_4 = I_1(\beta_1 a_1) K_1(\beta_1 a_2) - I_1(\beta_1 a_2) K_1(\beta_1 a_1) \end{split}$$

#### Dispersion relations, exact expressions

- $\frac{\varepsilon_1 \nu_0 J_0(\nu_0) W_3 + \nu_1 J_1(\nu_0) W_1}{\varepsilon_1 \nu_0 J_0(\nu_0) W_4 + \nu_1 J_1(\nu_0) W_2} + \frac{\varepsilon_1 \nu_2}{\varepsilon_2 \nu_1} \frac{H_0^{(1)}(\tilde{d}\nu_2)}{H_1^{(1)}(\tilde{d}\nu_2)} = 0$
- Here  $\tilde{d} = a_2/a_1$ ,  $v_0$  is the desired dimensionless transverse wavenumber in vacuum of the TM mode with zero first index;  $v_1$  and  $v_2$  transverse wavenumbers of the same mode in the inner layer and in the outer wall, respectively:  $v_{1,2} = \sqrt{k^2 a_1^2 (\varepsilon_{1,2} \mu_{1,2} 1) + v_0^2}$
- $W_1 = H_0^{(1)}(\nu_1) J_0(\tilde{d}\nu_1) J_0(\nu_1) H_0^{(1)}(\tilde{d}\nu_1)$
- $W_2 = -H_0^{(1)}(\nu_1)J_1(\tilde{d}\nu_1) + J_0(\nu_1)H_1^{(1)}(\tilde{d}\nu_1)$
- $W_3 = -H_1^{(1)}(\nu_1)J_0(\tilde{d}\nu_1) + J_1(\nu_1)H_0^{(1)}(\tilde{d}\nu_1)$
- $W_4 = H_1^{(1)}(\nu_1) J_1(\tilde{d}\nu_1) J_1(\nu_1) H_1^{(1)}(\tilde{d}\nu_1)$

for  $\sigma_2 \rightarrow \infty$ :

 $\varepsilon_1 \nu_0 J_0(\nu_0) W_3 + \nu_1 J_1(\nu_0) W_1 = 0$ 

Wake function: 
$$W_{||} = \int_{-\infty}^{\infty} Z_{||} e^{j\frac{\omega}{c}s} d\omega$$

## 3.Longitudinal Impedance, $a_1 = 2mm$ , $d = 200 \mu m$

- The next slide presents graphs of the longitudinal impedance of a metal-dielectric tube with a thick ( $d = 200 \mu m$ ) internal dielectric coating with relatively small values of the imaginary component of the dielectric constant ( $\varepsilon_1^{"}=0, 0.1, 0.5$ ) of the internal coating.
- A separate graph presents the impedance for the case of a relatively large  $(\varepsilon_1^{"}=3)$  imaginary component.
- Impedances are characterized by multiple resonant frequencies. The amplitudes of the impedances decrease with an increase of the imaginary component of the dielectric constant.

#### 3. Longitudinal Impedance, $a_1 = 2mm$ , $d = 200 \mu m$



## 4. Dispersion curves, $a_1 = 2mm$ , $d = 200\mu m$



In the absence of attenuation  $\varepsilon_1^{"}=0$  and at low attenuation  $\varepsilon_1^{"}=0.5$ , all resonant frequencies correspond to slowly propagating waveguide modes, the phase velocities of which are synchronous with the velocity of propagation of the particle and, therefore, affect to the movement of the test particle. The effect of higher resonant frequencies on the test particle can be countered by studying the shape of the corresponding wake functions.

## 5. Wake functions, $a_1 = 2mm$ , $d = 200 \mu m$

• The next slide shows the distributions of longitudinal wake functions for the following values of the imaginary component of the dielectric constant:  $\varepsilon_1^{"}=0$ , 0.1 and 0.5.

For  $\varepsilon_1^{"}=0$  and 0.1, the effect of higher resonant frequencies is significant throughout the presented maximal distance behind the particle ( $s \le 40mm$ ).

When  $\varepsilon_1^{"}=0.5$  their impact becomes insignificant already for s > 10mm. For these distances, in this case, the wakefield becomes monochromatic.

#### 5. Wake functions, $a_1 = 2mm$ , $d = 200\mu m$





With increasing attenuation the in while dielectric maintaining the fundamental resonant frequency, the contributions of higher resonant noticeable. frequencies With are increasing attenuation, their influence decreases.



## 6. Impacts of higher resonance frequencies

- The next two slides (9 and 10) show separately the contributions of the first three resonant frequencies to the wake function for cases  $\varepsilon_1^{"}=0$  and  $\varepsilon_1^{"}=0.5$ .
- In the first case (no attenuation,  $\varepsilon_1^{"}=0$ ), all three harmonics make a significant contribution to the total wakefield function. The sum of the three harmonics basically repeats the form of the full wake function, except for the immediate vicinity of the particle.
- In the second case, the convergence of harmonics to the full wake function is faster. Mainly the first two harmonics participate in the formation of the wake function.

## 6. Impacts of higher resonance frequencies, $\epsilon_1^{"}=0$



## 6. Impacts of higher resonance frequencies, $\epsilon_1^{"}=0.5$



## 7. Impedance, wake function and dispersion curves for the case of high attenuation $\epsilon_1^{"}=3$



For relatively large attenuation values in the presence of multiple resonances, only the main resonance frequency turns out to be in phase with the particle velocity. Phase velocities corresponding to higher harmonics turn out to be greater than the speed of light, i.e. rapidly propagating. However, in this case, the amplitude of the wake function decreases rapidly.

## 8. Case of thin dielectric cover, $d = 2\mu m$

Impedance





In this case, there is a single resonant frequency. The phase velocity of the harmonic at this frequency coincides with the velocity of the particle. As a result, the wakefield turns out to be monochromatic even in the immediate vicinity of the particle.

The advantage of a small thickness of the dielectric layer is also in the weak dependence of the wake field on the attenuation in the dielectric. The decrease in the amplitude of the wake function is mainly due to the finite conductivity of the outer wall.

### 8. Case of thin dielectric cover, $d = 2\mu m$

• For a thin lossless ( $\varepsilon_1'' = 0$ ) inner dielectric layer with an ideally conducting outer wall, the resonant frequency is determined by the expression

$$f_{rez} = \frac{c}{2\pi} \sqrt{\frac{\varepsilon_1'}{\varepsilon_1' - 1} \frac{2}{a_1 d}}$$

• The resonant frequency calculated using this formula for selected parameters gives  $f_{rez} = 1.1254 THz$ , whereas the same frequency calculated for the copper wall using exact formulas gives a slightly lower value  $f_{rez} = 1.1121 THz$ . The difference  $\Delta f_{rez} = 13.2 GHz$  is due to the finite conductivity of the outer copper wall



9. Transverse Impedance and Wake function. Thick inner cover  $a = 2mm, d = 200 \mu m, \epsilon'_1 = 10, \epsilon''_1 = 0$ 



10. Transverse Impedance and Wake function. Thin inner cover  $a = 2mm, d = 2\mu m, \epsilon'_1 = 10, \epsilon''_1 = 0$ 



There is only one resonance.

The wake function is harmonious

#### Dispersion curve. Thick inner cover $a = 2mm, d = 2\mu m, \epsilon'_1 = 10, \epsilon''_1 = 0; Mode TM_{11}$



#### Dispersion curve. Thick inner cover $a = 2mm, d = 2\mu m, \varepsilon'_1 = 10, \varepsilon''_1 = 0; Mode TM_{12}$



## Dispersion curve. Thin inner cover $a = 2mm, d = 2\mu m, \epsilon'_1 = 10, \epsilon''_1 = 0; Mode TM_{13}$



Curves do not intersect Coupling is weak

Conclusion: In the case of a thin coating, slowly propagating dipole modes are not generated. Generated modes have a phase velocity greater than the speed of light.

3.800

Thus, no effect of dipole modes on the transverse beam dynamics in the case of a thin internal dielectric coating 23

# 11. Case of Gaussian Bunch, rms length $\sigma = 0.5 ps (150 \mu m)$

Longitudinal wake potential



The presence of a bunch partially suppresses the contributions from higher modes, which in practice leads to the smoothing of additional bursts on the wake potential graph



## 12. CONCLUSION

- Studies have shown the possibility of optimal selection of the thickness and electromagnetic characteristics of the internal dielectric coating. For monochromatization of particle radiation, an important role is played the selection of the attenuation degree (selection of the optimal imaginary component of the dielectric constant of the dielectric). In particular, at  $\varepsilon_1 = 10$  and when the thickness of the inner layer is about 200 µm (that is, if the thickness is sufficiently large), the dielectric attenuation index should exceed 0.5 ( $tg\delta = 0.05$ ). On the other hand, the complete elimination of the influence of higher resonant frequencies can be avoided with attenuation greater than 3 ( $tg\delta = 0.3$ ). However, in this case, the amplitude of the wake function decreases rapidly.
- The preferred alternative is to use a thin dielectric coating with small attenuation. In this case, the equivalent circuit of the impedance of the structure is a parallel resonant oscillating circuit with the frequency-dependent complex shunt impedance and the emission of a particle is monochromatic, even in the immediate vicinity of it.
- The advantage of a small thickness of the dielectric layer is also in the weak dependence of the wake field on the attenuation in the dielectric. The decrease in the amplitude of the wake function is mainly due to the finite conductivity of the outer wall.
- Another advantage is the possibility of achieving high frequencies, since the resonant frequency is inversely proportional to the square of the layer thickness.
- No effect of dipole modes on the transverse beam dynamics in the case of a thin internal dielectric coating

## Thank you!